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Date: 10/16/07

To: USPTO  
 Basil Katchevs  
 Fax No.: 571-273-8300

From: OWSEM Initiative Group  
 Aleksandr Kamenomostskiy

No. of Pages: 12  
 (including this cover)

These materials relate to Patent Application No. 10/813,616, currently named "Thin-Webbed Profile Member and Panel Based on It", Publication No. US 2006/00181171, filed by the inventor Aleksandr Kamenomostskiy.

We are sending additional charts and graphs to better prove the criticality of dimension ratios of TWPMs' widths and thicknesses, claimed in application (a1 from 0.05 to 0.3 and a2 from 1 to 3).

The page 2 of this fax is a spreadsheet giving the value of  $\Sigma$  (Efficiency Factor) for the specific values of ratios of a1 and a2.

Page 3 is a two-dimensional chart for four values of a2 which shows the critical drop of value of  $\Sigma$  outside of claimed ranges.

Page 4 is a 3D-chart for all scope of data from the spreadsheet on page 2.

Pages 5 to 9 are the comparison data that display how the Alcoa's double-T profiles (I-Beams)

compare to TWPMs of the same shape for loads typical to aerospace applications. Inventor's calculations show that using the relationship  $\Sigma=f(a1,a2)$ , defined in the datasheet on page 2, a reduction of weight from 7% to 34% can be achieved.

Pages 10 to 12 are the letter that we recently sent to the office of SBDC NYS. Not having much time to edit it, we are including it as is. Please read chapters "An Introduction to the Application of OWSEM and its Benefits" and "Examples of Successful Implementations" to get better understanding of what this technology is about.

As we agreed on Tuesday, we will call you at 10:00 a.m. on Thursday October 18.

Look forward to speaking to you.

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$\Sigma$	a1																a2
	0	0.05	0.1	0.15	0.2	0.25	0.3	0.4	0.5	0.6	0.7	0.8	0.9	1	1.1	1.2	
0.5	0.48	0.48	0.5	0.51	0.5	0.48	0.48	0.42	0.37	0.34	0.3	0.26	0.23	0.21	0.2	0.19	1
0.55	0.48	0.5	0.51	0.51	0.5	0.48	0.47	0.42	0.38	0.35	0.32	0.28	0.25	0.24	0.23	0.22	1.1
0.6	0.48	0.5	0.51	0.51	0.51	0.49	0.47	0.43	0.39	0.36	0.32	0.29	0.27	0.24	0.24	0.23	1.2
0.65	0.48	0.5	0.51	0.51	0.51	0.49	0.47	0.43	0.39	0.36	0.32	0.29	0.28	0.26	0.26	0.25	1.3
0.7	0.48	0.5	0.51	0.51	0.51	0.49	0.47	0.43	0.39	0.36	0.32	0.29	0.28	0.27	0.27	0.26	1.4
0.75	0.48	0.5	0.51	0.52	0.51	0.49	0.47	0.43	0.4	0.36	0.33	0.3	0.28	0.27	0.27	0.26	1.5
0.8	0.48	0.51	0.52	0.52	0.51	0.5	0.47	0.43	0.4	0.37	0.33	0.31	0.28	0.27	0.27	0.26	1.6
0.85	0.48	0.51	0.52	0.52	0.51	0.5	0.47	0.43	0.4	0.37	0.33	0.31	0.28	0.27	0.27	0.26	1.7
0.9	0.48	0.51	0.52	0.52	0.51	0.5	0.47	0.43	0.4	0.37	0.33	0.31	0.28	0.27	0.27	0.26	1.8
0.95	0.48	0.52	0.52	0.52	0.51	0.5	0.47	0.43	0.4	0.37	0.33	0.31	0.28	0.27	0.27	0.26	1.9
1	0.48	0.52	0.52	0.52	0.51	0.5	0.47	0.43	0.4	0.37	0.33	0.31	0.28	0.27	0.27	0.26	2
1.1	0.48	0.52	0.52	0.52	0.51	0.5	0.47	0.43	0.4	0.37	0.33	0.31	0.28	0.27	0.27	0.26	2.1
1.2	0.48	0.52	0.52	0.52	0.51	0.5	0.47	0.43	0.4	0.37	0.33	0.31	0.28	0.27	0.27	0.26	2.2
1.3	0.48	0.52	0.52	0.52	0.51	0.5	0.47	0.43	0.4	0.37	0.33	0.31	0.28	0.27	0.27	0.26	2.3
1.4	0.48	0.52	0.52	0.52	0.51	0.5	0.47	0.43	0.4	0.37	0.33	0.31	0.28	0.27	0.27	0.26	2.4
1.5	0.48	0.52	0.52	0.52	0.51	0.5	0.47	0.43	0.4	0.37	0.33	0.31	0.28	0.27	0.27	0.26	2.5
1.6	0.48	0.52	0.52	0.52	0.51	0.5	0.47	0.43	0.4	0.37	0.33	0.31	0.28	0.27	0.27	0.26	2.6
1.7	0.48	0.52	0.52	0.52	0.51	0.5	0.47	0.43	0.4	0.37	0.33	0.31	0.28	0.27	0.27	0.26	2.7
1.8	0.48	0.52	0.52	0.52	0.51	0.5	0.47	0.43	0.4	0.37	0.33	0.31	0.28	0.27	0.27	0.26	2.8
1.9	0.48	0.52	0.52	0.52	0.51	0.5	0.47	0.43	0.4	0.37	0.33	0.31	0.28	0.27	0.27	0.26	2.9
2	0.48	0.52	0.52	0.52	0.51	0.5	0.47	0.43	0.4	0.37	0.33	0.31	0.28	0.27	0.27	0.26	3
2.1	0.48	0.52	0.52	0.52	0.51	0.5	0.47	0.43	0.4	0.37	0.33	0.31	0.28	0.27	0.27	0.26	3.1
2.2	0.48	0.52	0.52	0.52	0.51	0.5	0.47	0.43	0.4	0.37	0.33	0.31	0.28	0.27	0.27	0.26	3.2
2.3	0.48	0.52	0.52	0.52	0.51	0.5	0.47	0.43	0.4	0.37	0.33	0.31	0.28	0.27	0.27	0.26	3.3
2.4	0.48	0.52	0.52	0.52	0.51	0.5	0.47	0.43	0.4	0.37	0.33	0.31	0.28	0.27	0.27	0.26	3.4
2.5	0.48	0.52	0.52	0.52	0.51	0.5	0.47	0.43	0.4	0.37	0.33	0.31	0.28	0.27	0.27	0.26	3.5
2.6	0.48	0.52	0.52	0.52	0.51	0.5	0.47	0.43	0.4	0.37	0.33	0.31	0.28	0.27	0.27	0.26	3.6
2.7	0.48	0.52	0.52	0.52	0.51	0.5	0.47	0.43	0.4	0.37	0.33	0.31	0.28	0.27	0.27	0.26	3.7
2.8	0.48	0.52	0.52	0.52	0.51	0.5	0.47	0.43	0.4	0.37	0.33	0.31	0.28	0.27	0.27	0.26	3.8
2.9	0.48	0.52	0.52	0.52	0.51	0.5	0.47	0.43	0.4	0.37	0.33	0.31	0.28	0.27	0.27	0.26	3.9
3	0.48	0.52	0.52	0.52	0.51	0.5	0.47	0.43	0.4	0.37	0.33	0.31	0.28	0.27	0.27	0.26	4